

## AC-TO-AC POWER CONVERTER WITHOUT A DC LINK CAPACITOR

5

### BACKGROUND OF THE INVENTION

The present invention relates to electrical power conversion systems. More specifically, the present invention relates to an ac-to-ac converter.

Many aircraft include electric drives, ac distribution systems and ac-to-ac converters. Typically, the ac-to-ac converter converts ac power from the distribution system to a frequency that is suitable for operating an electric drive.

Two basic types of converters are usually used to perform the ac-to-ac conversion in aircraft. The first type of converter includes a source-side inverter for converting ac source power to dc power and supplying the dc power to a dc link; a low-impedance dc link capacitor connected across the dc link for smoothing dc link voltage; and a drive-side inverter for converting the dc power on the dc link to ac power.

The dc link capacitor tends to be large and heavy. Moreover, both the source-side and drive-side inverters are switched at high frequencies, which leads to high switching losses.

The second type of converter includes a single so-called "matrix" inverter. The matrix inverter does not have a dc link or a dc link capacitor. However, the matrix inverter includes more switches than the first type of converter (for three-phase power conversion, a typical matrix inverter includes 50% more switches). The additional switches make the matrix inverter more expensive. Moreover, switching of the matrix inverter is more difficult to control due to the greater number of switches, and the switching logic is more complex.

It would be desirable to eliminate the dc link capacitor in the first

type of converter. Eliminating the dc link capacitor would reduce the weight, which, in turn, would reduce aircraft fuel consumption and aircraft operating costs.

5 It would also be desirable to reduce the switching losses in the first type of converter. Simplifying the switching and reducing the switching frequency would reduce switching losses.

#### SUMMARY OF THE INVENTION

10 According to one aspect of the present invention, an ac-to-ac converter includes a source-side inverter; a drive-side inverter; a dc current link coupled between the source-side inverter and the drive-side inverter; and a controller for operating the source-side inverter in current mode and the drive-side inverter in commutation mode.

15 Switching of the drive-side inverter is simple. High frequency switching is performed in the source-side inverter only. Moreover, the converter does not need a large dc link capacitor.

#### BRIEF DESCRIPTION OF THE DRAWINGS

20 Figure 1 is an illustration of a system including an ac distribution system, an ac-to-ac power converter and an electric motor;

Figures 1a and 1b are illustrations of switches for source-side and drive-side inverters of the power converter;

Figure 2 is an illustration of a modulating cycle for the source-side inverter;

25 Figure 3 is a diagram of possible vectors during current mode space-vector modulation;

Figure 4 is an illustration of a source-side controller for the source-side inverter;

30 Figure 5 is an illustration of a damping circuit for the source-side controller;

Figure 6 is an illustration of a drive-side controller for the drive-side inverter; and

Figure 7 is an illustration of an ac-to-ac converter including a bridge rectifier for bi-directional power flow.

5

### DETAILED DESCRIPTION OF THE INVENTION

Referring to Figure 1, a system 10 includes an ac power source 12, an ac-to-ac power converter 14 and an electric motor 16. The ac power source 12 supplies three-phase ac power at a first frequency, and the ac-to-ac converter 14 converts the ac power to a second frequency that is suitable for the electric motor 16. In an aircraft, for example, the ac power source 12 might include an ac distribution system that provides three-phase 400 Hz ac power, and the motor 16 may be a permanent magnet ac motor for a compressor. The ac-to-ac converter converts the 400 Hz ac power to variable frequency power and supplies the variable frequency power to the ac motor.

The ac-to-ac converter 14 includes a "source-side" solid-state inverter 18, a "drive-side" solid-state inverter 20 and a dc current link 22 coupled between an output of the source-side inverter 18 and an input of the drive-side inverter 20. The source-side inverter 18 includes six switches 24: each inverter phase includes two switches 24 (an upper switch and a lower switch). Each switch 24 of the source-side inverter 18 includes a controllable solid-state device (e.g., an IGBT or MOSFET device) 24a and a diode 24b (see Figure 1a). The drive-side inverter 20 also includes six switches 26: each inverter phase includes two switches 26 (an upper switch and a lower switch). Each switch 26 of the drive-side inverter 20 includes a controllable solid-state device (e.g., an IGBT or MOSFET device) 26a and a diode 26b (see Figure 1b).

The ac-to-ac converter 14 is terminated in a three-phase capacitor bank 27 at the source side. The capacitor bank 27 supplies a low source

impedance to the inverters 18 and 20, supplying current when two switches 24 in different phases of the source side inverter 18 are closed. When two switches 24 in the same phase of the source-side inverter 18 are closed, the dc link current freewheels through the shorted phase of the source-side inverter 18, and no current is extracted from the capacitor bank 27. In addition, the capacitor bank 27 provides EMI protection.

The ac-to-ac converter 14 also includes a source-side controller 28a for controlling the source-side inverter 18 in a current mode and a drive-side controller 28b for controlling the drive-side inverter 20 in a commutation mode. While the source-side inverter 18 is operated in current mode, only two of its six switches 24 conduct current at any time. While the drive-side inverter 20 is operated in commutation mode, only three of its six switches 26 conduct current at any time. Switching of the drive-side inverter 20 is performed at 60-degree intervals relative to the fundamental frequency of the motor 16. This makes for a simple control.

The source-side inverter 18 is modulated at a high frequency (e.g., 20-40 kHz for 400 Hz power). Switching of the source side inverter 18 is performed at frequency that is compatible with the type of power switch being used, (for example, 20KHz for an IGBT). The frequency is selected to minimize ripple on the drive side, which depends upon the inductance of the motor 16. Increasing the switching frequency reduces the size of the capacitor bank 27 but increases the switching loss for the source-side inverter switches 24.

Reference is now made to Figure 2, which shows a modulating cycle for the source-side inverter 18. Each modulating cycle of the source-side inverter has a period TSVM. Each modulating cycle includes a current regulation portion DC, which has a first duty cycle d01. The current regulation portion DC is that portion of the modulation cycle required to control the average current in the dc link 22. During the current regulation portion DC of each modulating cycle, the source-side inverter

18 may be controlled as a current-regulated buck (down) chopper to maintain a controlled, constant current on the dc current link 22. The source-side controller 28a commands the switches 24 of the source-side inverter 18 to short the dc link 22 (both top and bottom switches 24 of a single inverter phase are closed) for the specified duty cycle d01.

Each modulating cycle also includes a Space-vector modulation ("SVM") portion MOD, which includes duty cycles d02, d1 and d2. The order in which the duty cycles are arranged is arbitrary. This SVM portion MOD is controlled to provide sinusoidal currents sourced from the supply side. During the SVM portion of each modulating cycle MOD, the source-side controller 28a modulates the six switches of the source-side inverter 18 at a high frequency to extract fundamental frequency sinusoidal currents (with high order harmonic currents due to the modulating process) from the ac power source 12. Resulting on the dc current link 22 is essentially a constant dc current with high frequency components at six times the fundamental frequency of the ac power source 12 (and its associated harmonics) and at the modulating frequency (and its associated harmonics).

Reference is made to Figure 3, which shows a null vector and six possible current Park vectors I1 to I6 for current mode SVM. Park vectors inherently contain information on both the instantaneous magnitudes and the phase relationship of three phase rotating fields with respect to a reference coordinate system. A Park vector, in general, is a mathematical representation that describes the locus of an electrical quantity in the complex space domain (where time is a parameter). A current Park vector is defined with the vector's amplitude and the vector's direction in spatial relation to the three phases. A general discussion of Park vectors is provided in P.K. Kovacs, "Transient Phenomena in Electrical Machines," Elsevier Science Publishing Co. (1984).

Each current Park vector is displaced by 60 electrical degrees, and

is produced by closing two switches in different phases of the source-side inverter 18. The null vector results from the two switches 24 in a single phase being closed, or from all switches 24 being open. For example, the null vector can occur when all switches 24 of the source-side inverter 18 are open, or when the top and bottom switches 24 of a single phase of the source-side inverter 18 are turned on, essentially short-circuiting the dc current link 22 and allowing the current to circulate through the shorted phase.

The source-side controller 28a varies the duty cycles  $d_1$  and  $d_2$  and selects the current vectors  $i_{k1}$  and  $i_{k2}$  (and the null vector) to create a rotating current vector  $I_{AVG}$ . The duty cycles  $d_1$  and  $d_2$  are selected to produce a sinusoidal current that best matches the dc link current that is required by the motor 16. Typical SVM algorithms relate the current vector  $I_{AVG}$  to the duty cycles  $d_1$ ,  $d_2$  and  $d_{02}$  with the corresponding  $i_{k1}$ ,  $i_{k2}$  and null current Park vectors. In other words, the vector  $I_{AVG}$  is a time averaged composite vector of the  $i_{k1}$ ,  $i_{k2}$  and null current vectors during each SVM portion.

The source-side controller 28a uses the current vector  $I_{AVG}$  to command the source-side inverter switches 24 to connect selected phases of the capacitor bank capacitors to the dc current link 22 and maintain a relatively ripple-free current on the dc link. Magnitude of the desired inverter current vector  $I_{AVG}$  is essentially determined by the requirements of the motor 16, and relates directly to the torque that is being controlled by the motor 16. The angle of the desired inverter current vector  $I_{AVG}$  is determined by the voltage vector derived from the capacitor bank 27. A unity power factor at the capacitor bank 27 would require the angle of the inverter current vector  $I_{AVG}$  to be equal to the angle of the capacitor bank voltage vector.

The duty cycles  $d_{01}$  and  $d_{02}$  comprise the total null vector when either the top and bottom switches 24 of a single phase of the source-side

inverter 18 are turned on, or when all of the switches 24 are open. In either case, no current is transferred between the source and the drive-side inverter 20 during the duty cycles d01 and d02. The average amplitude of the dc current is controlled by the duty cycle d01. The duty cycle d02 is determined by the SVM algorithm, so that essentially sinusoidal fundamental currents result in the ac distribution side, with higher order harmonics superimposed from the modulating frequency.

Reference is now made to Figure 4, which shows the source-side controller 28a in greater detail. The source-side controller 28a includes a summing junction 29 for comparing a current command IdCCMD to current feedback Ifb from the dc link 24, and passing the resultant error to a dc current regulator 30, which regulates the dc current link current. This regulator 30 is typically a proportional integral regulator.

The dc regulator 30 provides a duty cycle command Cd01 to gate logic 34 and SVM logic 36. A voltage Park vector VCAP of the capacitor bank 27 is computed (block 37). The voltage Park vector VCAP may be computed from the sensed line to neutral voltages (or line to line voltages) sensed at the capacitor bank 27. The angle ANG of this voltage Park vector VCAP is also supplied to the SVM logic 36.

The SVM logic 36 selects the appropriate current vectors I1-I6 (Figure 3), and computes and apportions the duty cycle commands Cd1, Cd2, and Cd02, based upon the remaining duty cycle (TSVM-d01) (Figure 2) so that a sinusoidal current vector results in the supply-side source 12. The duty cycle commands Cd1, Cd2 and Cd02 are supplied to the gate logic.

The source-side controller 28a may also include a damping circuit 40. Damping is usually performed so that the input inductance and capacitance of the source side inverter 20 is not excited at its resonant frequency by current harmonics that are injected into the power source 12 by non-linear loads. Damping may be accomplished by a damped

0975054-011001

inductor or a resistor-capacitor combination or by active damping.

Figure 5 shows an exemplary damping circuit 40 in greater detail. The voltage Park vector  $V_{CAP}$  is operated upon by a low pass filter (LPF) 42, which provides a vector  $V_{FUND}$  representing the fundamental of the capacitor bank voltage 27. The voltage Park vector  $V_{CAP}$  and the vector from the LPF 42 are applied to a summing junction 44, which provides a difference vector  $V_{DIF}$ , representing any resonant frequencies of the voltage Park vector  $V_{CAP}$ . The difference vector  $V_{DIF}$  is compared to a zero reference by another summing junction 46, and the resulting error signal  $V_{ERR}$  is applied to a proportional regulator 48 whose output provides a signal  $da$  representing an incremental angle. The incremental angle is a corrective term that modifies the capacitor bank voltage Park vector angle  $ANG$  to minimize harmonic content on the capacitor bank 27.

As mentioned above, the drive-side controller 28b controls the drive-side inverter 20 in the commutation mode. A drive-side inverter 20 having six switches 26 will have a total of eight possible switching states when one switch 26 in each leg is conducting. Six of these switching states - which occur when power is transferred from the link 22 to the motor 16 or from the motor 16 to the link 22 - may be described by six so-called "active" vectors. The remaining two switching states - which occur when all three upper switches 26 are conducting at the same time or all three lower switches 26 are conducting at the same time - may be described by null vectors. When all three upper switches 26 are conducting at the same time or all three lower switches 26 are conducting at the same time, the motor 16 is effectively isolated from the link 22.

The drive-side controller 28b commands the drive-side inverter 20 to generate active vectors only. The null vectors are imposed on the drive-side inverter 20 by the source-side inverter 18. A null vector on the drive-side inverter 20 results when the source side inverter 18 is commanded to produce a null vector. If the source-side inverter 18



commands all switches 24 off, current in the motor 16 will freewheel such that a null vector appears on the motor load. If the source-side inverter 18 commands a null vector by shorting the dc link 22, some of the motor current will freewheel through the drive-side inverter switches 26 of the shorted phase, and apply a null vector to the motor 16.

Control of the drive-side inverter 20 is limited to determining the time to commute the drive-side inverter 20 from one motor current vector to another in order to maintain constant unity power factor at the inverter 20 and the terminals of the motor 16. With the drive-side inverter 20 maintaining a constant power factor, the source-side inverter 18 controls the amplitude of the current and, therefore, the torque, while at the same time, producing ac sinusoidal currents from the ac power source 12.

For example, the drive-side controller 28b causes the drive-side inverter 20 to perform the commutation at 6x fundamental frequency of the load at the motor 16. Switching frequency of the drive side inverter switches 26 is only a function of motor frequency, not the frequency at the source side.

Reference is now made to Figure 6, which shows an exemplary drive-side controller 28b in greater detail. Power factor control may be performed as follows for a motor 16 having rotor position sensors. These position sensors, which may be Hall effect devices or other types of sensors, are adjusted to be in phase with the emf vector of the motor 16. The position sensors generate a signal RTR that provides information for computing a rotor position unit vector  $e^{(-jn\pi/3)}$ , where n is the rotor segment (block 102). For n=1,6 there are six discrete angles that are displaced 60 degrees from one another.

A Park vector IMTR of motor stator current is also computed (block 104). This Park vector IMTR may be derived by sampling the motor stator three phase currents (ia, ib, ic) at the switching frequency of the source-side inverter 18.

The rotor position unit vector  $e^{(-jn\pi/3)}$  is used to achieve a coordinate transformation of the stator current Park vector  $IMTR$  of the motor 16 (block 106). Transformation to the synchronous reference frame is accomplished by multiplying the motor current Park vector  $IMTR$  by the unit vector  $e^{(-jn\pi/3)}$ .

5        The imaginary portion of the resultant vector is extracted (block 108) and compared to a reference, usually zero (block 110). The error is operated upon by a proportional integral power factor regulator 112, whose output is summed with the rotor position signal  $RTR$  (block 114). This shifts the rotor position signal  $RTR$  by an angle  $\theta$ . The shifted rotor position signal is used as a commutation vector  $V_c$  by inverter logic 116 to select the appropriate Park vector which, in turn, selects the states of the six switches 26 of the drive-side inverter 20. The rotor position signal is shifted to reduce the imaginary component of the motor current Park vector  $IMTR$  to zero. In this way, the power factor is regulated at the terminals of the motor such that the motor current is in phase with the back emf.

15        The controllers 28a and 28b may be software or hardware implementations or a combination of the two.

20        Thus disclosed is an ac-to-ac converter 14 in which switching of the drive-side inverter 20 is simple to control. High frequency (e.g., 20 kHz) switching is performed in the source-side inverter 18 only. Moreover, the ac-to-ac converter 14 does not need a large dc link capacitor on the dc current link to perform the ac-to-ac conversion.

25        Although the system 10 has been described in connection with an electric motor 16, it is generally applicable to any drive. Although the system 10 has been described in connection with three-phase ac power, it is not so limited.

30        Power flow in the ac-to-ac converter 10 of Figure 1 is uni-directional. However, power flow may be made bi-directional by adding a diode bridge to the dc current link (see Figure 7). This addition enables

the source-side inverter 18 to maintain the same current direction with an inverted voltage obtained from the capacitor bank capacitors, while at the same time providing a current reversal on the drive-side inverter 20, while maintaining the same voltage polarity.

- 5           The ac-to-ac converter is not limited to the specific embodiment described above. Instead, the invention is construed according to the claims that follow.

050-99-050